

Microalgae bio-reactive façade: location and weather-based systematic optimization

Supplementary materials

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Thermal model

The model is based on a heat balance between the biofaçade reservoir and its surrounding. It comprises:

- incident direct solar radiation (Φ_{Sun} , split into infrared radiation and visible light, Eq. 1). $\Phi_{Sun,Vis}$, being determined by the model proposed by the Illuminating Engineering Society (1), accounts for 48.7 % of total sun power (2), which allows to derive $\Phi_{Sun,IR}$ (Eq. 2),
- sky radiation (Eq. 3, 4, 5, and 6), calculated using a sky temperature model (3–5),
- surrounding radiation (Eq. 9, 10, 11, 12 and 13), accounting for Urban Heat Island effect (6–9),
- controlled absorption of the visible part of the radiative heat flux (Eq. 7) and associated reflectivities (Eq. 8) (10),
- indoor radiation (Eq. 14 and 15) (11),
- indoor convection using resistance in series modeling approach (Eq. 16, 17, and 18) (4, 11, 12),
- outdoor convection using resistance in series modeling approach (Eq. 19, 20, 21, and 22) and Defraeye's correlation to assess wind contribution (Table 1) (13, 14),
- power originated from the gas sparged into the reservoir (Eq. 23).

Combined together, they govern the temporal evolution of the biofaçade reservoir temperature (Eq. 24).

$$\Phi_{Sun} = \Phi_{Sun,Vis} + \Phi_{Sun,IR} \quad (1)$$

$$\Phi_{Sun,IR} = \left(\frac{1}{0.487} - 1\right)\Phi_{Sun,Vis} = 1.05\Phi_{Sun,Vis} \quad (2)$$

$$\Phi_{Sky,Tot} = \sigma\epsilon_{Sky}T_{Sky}^4 \quad (3)$$

$$\begin{aligned} \epsilon_{Sky}T_{Sky}^4 &= 9.36575 \cdot 10^{-6}(1 - CC)T_{Air,Out}^6 \\ &+ T_{Air,Out}^4 CC \left[(1 - 0.84CC)(0.527 + 0.161 \exp(8.45[1 - \frac{273}{T_{Air,Out}}])) + 0.84CC \right] \end{aligned} \quad (4)$$

$$\Phi_{Sky,Abs} = F_{Sky}(0.4 \tau_{Sun} + 0.6 \tau_{Sky,Abs}) \left(\frac{3 - 2\alpha^2 - \alpha}{3} (1 - \eta_{ps}) \Phi_{Sky,Vis} + (\Phi_{Sky,Tot} - \Phi_{Sky,Vis}) \right) \quad (5)$$

$$\Phi_{Sky,Emi} = F_{Sky}\tau_{Sky,Emi}\sigma\epsilon_{mc}T_{mc}^4 \quad (6)$$

$$\Phi_{Sun,Abs} = \tau_{Sun} \left(\frac{3 - 2\alpha^2 - \alpha}{3} (1 - \eta_{ps}) \Phi_{Sun,Vis} + 1.05\Phi_{Sun,Vis} \right) \quad (7)$$

$$R_{interface} = \frac{1}{2} \left[\frac{\tan^2(\theta_i - \theta_r)}{\tan^2(\theta_i + \theta_r)} + \frac{\sin^2(\theta_i - \theta_r)}{\sin^2(\theta_i + \theta_r)} \right] \quad (8)$$

$$UHII = \max(T_{Urb} - T_{Rur}) \quad (9)$$

$$UHII = -0.54 \bar{U} - 1.48 \overline{CC} - 0.039 \bar{Y} + 7.63 \quad (10)$$

$$T_{Rur} = (1 - CC)(2.82 + 1.15T_{Air,Out}) + CC(1.33 + 1.00T_{Air,Out}) \quad (11)$$

$$\Phi_{Sur,Abs} = F_{Sur} \tau_{Sur,Abs} \sigma \epsilon_{Sur} T_{Sur}^4 \quad (12)$$

$$\Phi_{Sur,Emi} = F_{Sur} \tau_{Sur,Emi} \sigma \epsilon_{mc} T_{mc}^4 \quad (13)$$

$$\Phi_{In,Rad,Abs} = \tau_{In,Rad,Abs} \sigma \epsilon_{In} T_{In}^4 \quad (14)$$

$$\Phi_{In,Rad,Emi} = \tau_{In,Rad,Emi} \sigma \epsilon_{mc} T_{mc}^4 \quad (15)$$

$$h_{In,Conv,Free} = 2.04 \left(\frac{H_{mc}}{H_{Ref,In}} (T_{pmma,In} - T_{Air,In}) \right)^{0.23} \quad (16)$$

$$h_{In,Conv,Forced} = \frac{k_{Air}}{L_{Ref}} 0.664 Re_{Ref}^{1/2} Pr^{1/3} = 0.72 \text{ W/m}^2/\text{K} \quad (17)$$

$$\Phi_{In,Conv,Net} = \frac{T_{Air,In} - T_{mc}}{\frac{1}{h_{In,Conv}} + \frac{e_{pmma}}{k_{pmma}}} \quad (18)$$

$$\frac{1}{h_{Out,Conv,Free}} = \frac{k_{Air}}{E_{mc}} \left[0.825 + \frac{0.387 Ra_L^{1/6}}{[1 + (0.492 Pr)^{9/16}]^{8/27}} \right]^2 \quad (19)$$

$$U_{Out} = U_{Station} \left(\frac{r_{Building}}{r_{Station}} \right)^{0.0706} \frac{\ln\left(\frac{E_{mc} + r_{Building}}{r_{Building}}\right)}{\ln\left(\frac{E_{Station} + r_{Station}}{r_{Station}}\right)} \quad (20)$$

$$h_{Out,Conv,Forced} = A_{\theta_{Wind}} U_{Out}^{B_{\theta_{Wind}}} \quad (21)$$

Wind incidence angle (θ_{Wind} , in degree)	$A_{\theta_{Wind}}$ (W/m ² /K)	$B_{\theta_{Wind}}$ (-)
0	4.90	0.86
30, 330	4.63	0.87
30, 300	4.25	0.88
90, 270	2.78	0.87
120, 240	1.44	0.83
150, 210	1.85	0.84
180	2.25	0.84

Table 1. Defraeye's correlation for different wind incidence angles on the facade. Couples of incidence angles tied to the same parameters originate from symmetry consideration

$$\Phi_{Out,Conv,Net} = \frac{T_{Air,Out} - T_{mc}}{\frac{1}{h_{Out,Conv}} + \frac{n_{Glaz} e_{pmma}}{k_{pmma}} + \frac{(n_{Glaz} - 1) e_{Air}}{k_{Air}}} \quad (22)$$

$$P_{Gas,Net} = f H_{mc} w_{mc} e_{mc} \rho_{Gas} C_{pGas} (T_{Gas} - T_{mc}) \quad (23)$$

$$H_{mc} w_{mc} e_{mc} \rho_{Water} C_{pWater} \frac{dT_{mc}}{dt} = H_{mc} w_{mc} [\Phi_{Sun,Abs} + \Phi_{Sky,Abs} - \Phi_{Sky,Emi} + \Phi_{Sur,Abs} - \Phi_{Sur,Emi} + \Phi_{In,Rad,Abs} - \Phi_{In,Rad,Emi} + \Phi_{In,Conv,Net} + \Phi_{Out,Conv,Net}] + P_{Gas,Net} \quad (24)$$

Performance distribution convergence analysis

Figure 1 reports the arithmetic mean and the standard deviation of the performance criteria as a function of the number of draws in the Sobol's sequence. As one can see, 2^8 draws are required to ensure a 10 % convergence on both the arithmetic mean and the standard deviation.

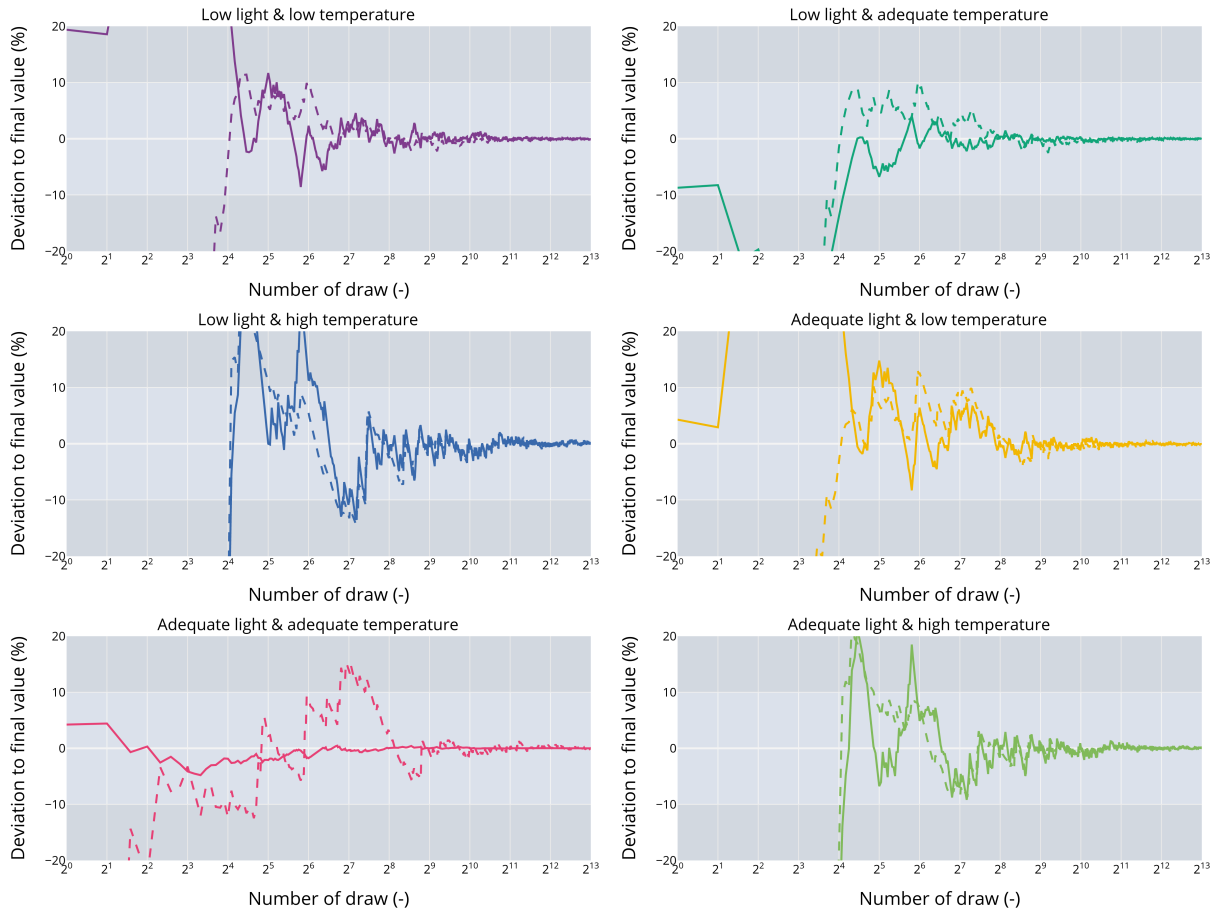


Fig. 1. Performance distribution arithmetic mean and standard deviation as function of the number of draw in the Sobol's sequence

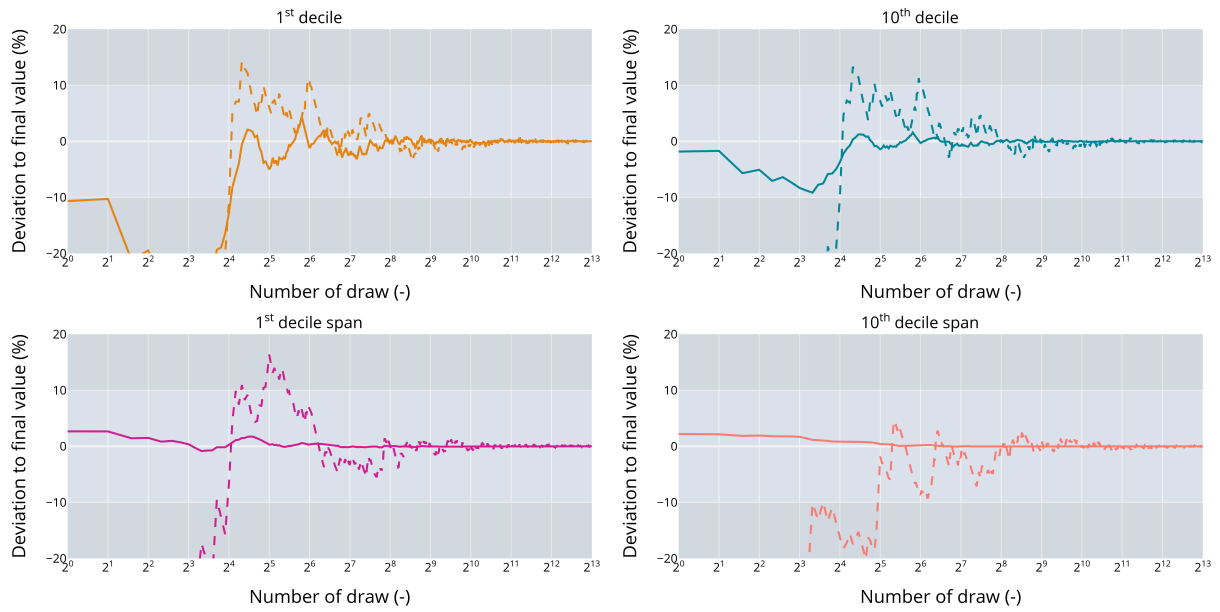


Fig. 1 (continued)

Nomenclature

Latin symbols	Property	Unit
A	First parameter of Defraeye's correlation	-
B	Second parameter of Defraeye's correlation	W/m ² /K
CC	Cloud Cover factor	-
C _p	Specific heat	J/kg/K
E	Elevation above the ground	m
e	Thickness	m
F	View factor	-
f	Arealation	VVM (Vessel Volume per Minute)
H	Height	m
h	Convective heat transfer coefficient	W/m ² /K
k	Thermal conductivity	W/m/K
L	Characteristic length	m
n _X	Number of X	-
P	Power	W
Pr	Prandtl number	-
Re	Reynolds number	-
R	Reflectivity	-
Ra	Rayleigh number	-
r	Surface roughness	m
T	Temperature	°C in the text / K in formulas
t	Time	s
U	Velocity	m/s
UHII	Urban Heat Island Intensity	K
w	Width	m
Y	Relative humidity	%

Greek symbols	Property	Unit
α	Green light transmitted fraction	-
ϵ	Emissivity	-
η	Efficiency	-
θ	Angle	rad
ρ	Density	kg/m ³
σ	Boltzmann's constant	W/m ² /K ⁴
τ	Transmission	-
Φ	Heat flux	W/m ²

Subscript	Description
Abs	Absorbed by the culture
Air	Air, indoor or outdoor
Building	Building hosting the facade
Conv	Convective-conductive
Emi	Emitted
Forced	Forced convection
Free	Free convection
Gas	Sparged gas
Glaz	Glazing
i	Incidence
In	Indoor
Interface	Interface
IR	Infrared
mc	Microalgae culture
Net	Net exchange
Out	Outdoor
pmma	PolyMethyl MethAcrylate
ps	Photosynthesis
r	Refraction
Rad	Radiative
Ref	Reference
Rur	Rural
Sky	Sky
Station	Meteorological station
Sun	Sun
Sur	Surrounding
Tot	Total
Urb	Urban
Vis	Visible
Water	Water
Wind	Wind

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